

Improving Phase Noise of PLLs at Low Frequencies

Introduction

Peregrine Semiconductor's integer-N and fractional-N PLL frequency synthesizers deliver superior phase noise performance where ultra-low phase noise is critical. However, as the edge rate of the RF input signal decreases, the phase noise will begin to degrade. At this point, the best performance for phase noise is obtained for signals with a higher slew rate, such as a square wave.

This application note describes the prescaler bypass mode for low frequency operation and presents a method to improve the phase noise. This application note focuses on the PE97240 integer-N phase locked loop (PLL) frequency synthesizer, but can be applied to all Peregrine Semiconductor PLL products.

Summary

- Prescaler bypass mode supports low frequency operation.
- Phase noise will degrade as the slew rate RF input signal decreases below the minimum value.
- The RF input frequency may be decreased while maintaining the minimum slew rate.

Normal Operating Mode

The main counter chain of Peregrine's PLL products divides the RF input frequency (F_{IN}) by an integer or fractional number derived from the values in the M and A counters, and the DSM input word K where applicable. Under normal operating conditions, the PE97240 has an RF frequency output range up to 5 GHz and a typical normalized phase noise floor of -230 dBc/Hz^{*}. The prescaler input requires a 0 dBm minimum input power level for optimal phase noise performance when a sine wave is applied at a minimum slew rate of 4 V/ns.

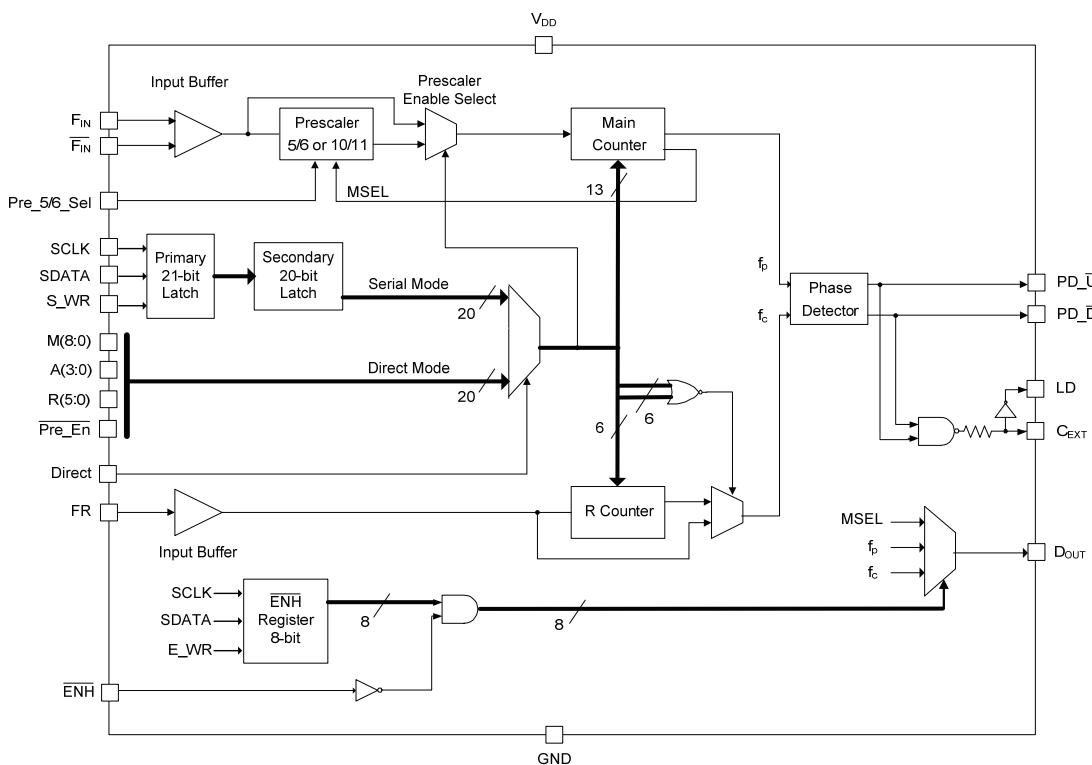
The minimum RF input frequency specified for the PE97240 is 800 MHz under normal operation. The lower frequency specification of the prescaler is determined by the minimum slew rate requirement. In theory, it is possible to operate the PLL at a lower input frequency by increasing the input power. The prescaler uses static logic so there is no reason why it wouldn't work down to DC. However, as the frequency decreases, there is a point where the minimum power level required becomes impractical. For example, if the minimum input power required is close to the specified maximum input power. When using the part below 800 MHz, it is recommended to use prescaler bypass mode.

Note: * Normalized phase noise is a figure of merit (FOM) often found in datasheets. Normalized PN = $PN_{FLOOR} - 20\log_{10}(f_{VCO}/f_c) - 10\log_{10}(f_c)$.

Prescaler Bypass Mode

Setting the Pre_En pin "high" allows F_{IN} to bypass and power down the prescaler as indicated in the block diagram in *Figure 1*. In this mode, the prescaler and the A register are not active, and the input VCO frequency is divided by the M counter directly.

Figure 1. PE97240 Functional Block Diagram



The operating frequency of the PE97240 in prescaler bypass mode is 50 MHz to 800 MHz. Prescaler bypass mode can handle a slower slew rate and is recommended for lower VCO frequencies to realize the same phase noise as compared to normal operating mode. However, as the frequency decreases, it becomes difficult to keep up with minimum edge rate required using a sine wave. As the slew rate of the input signal decreases, at some point the phase noise will start to degrade. For example, a slew rate of 4 V/ns at 325 MHz is equivalent to a sine wave with amplitude of $2 V_{PK}$. This level would exceed the maximum input power specification of the main divider. In order to maintain good phase noise performance, it is necessary to increase the edge rate of the RF input signal.

Application Example

Figure 2 shows a possible solution for a clock cleaning application where a PLL may be used to recover a noisy clock. In this example, the VCO supplies a low noise 100 MHz sine wave to the RF input of the PLL.

Figure 2. Block Diagram of 100 MHz PLL Test Circuit

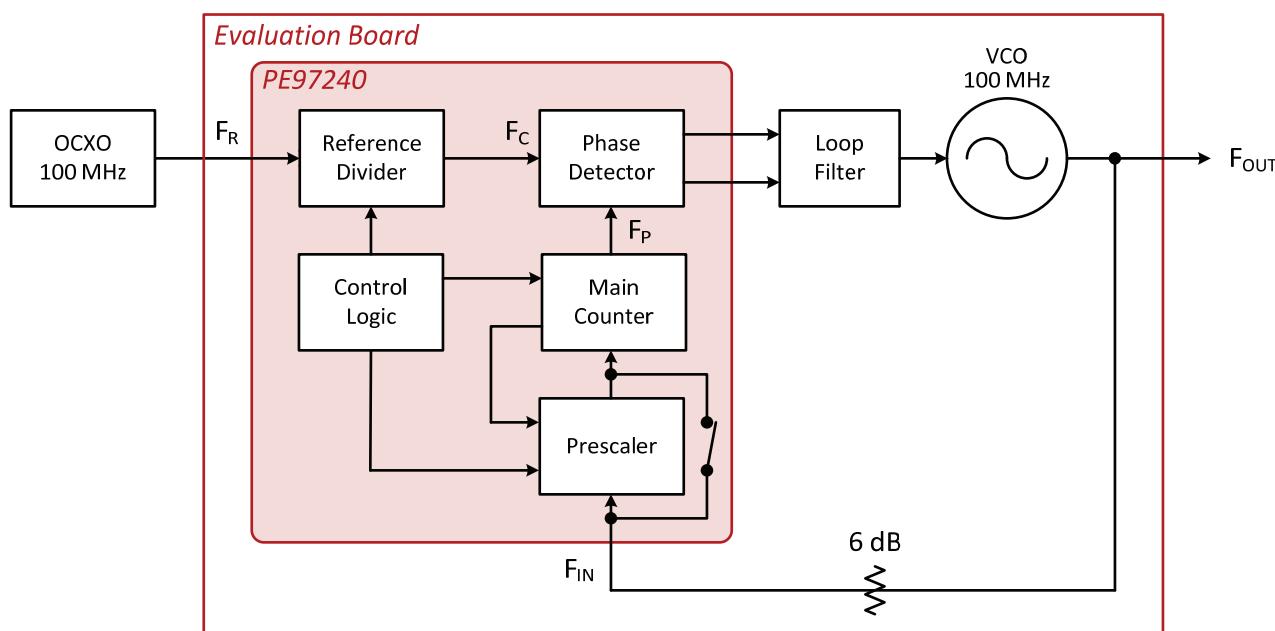
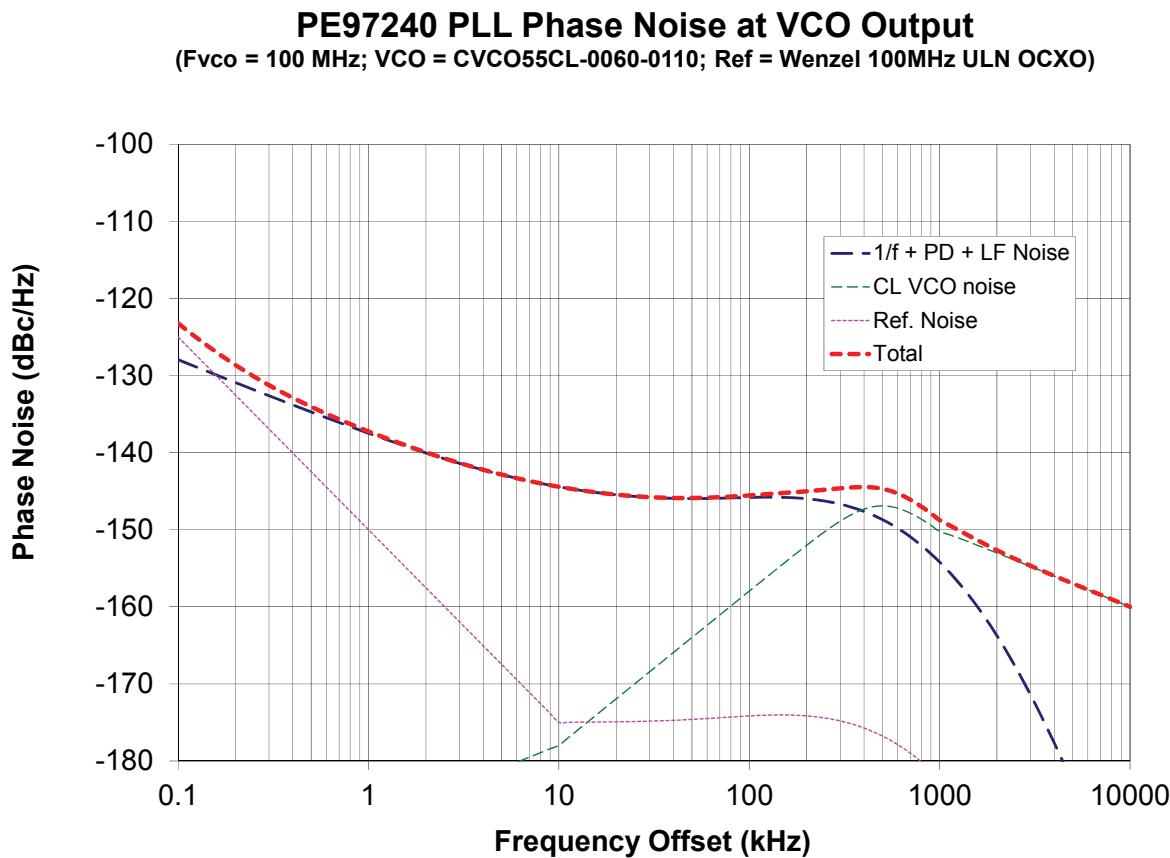


Figure 3 shows the simulated phase noise performance using the PE97240 PLL loop filter calculator and phase noise estimator spreadsheet*. In this example, the reference frequency (F_R) is 100 MHz, the comparison frequency (F_C) is 50 MHz and the loop bandwidth is 500 kHz. The loop bandwidth is extended in order to determine the normalized phase noise. Measuring the phase noise with a wider loop bandwidth more accurately captures the PLL.

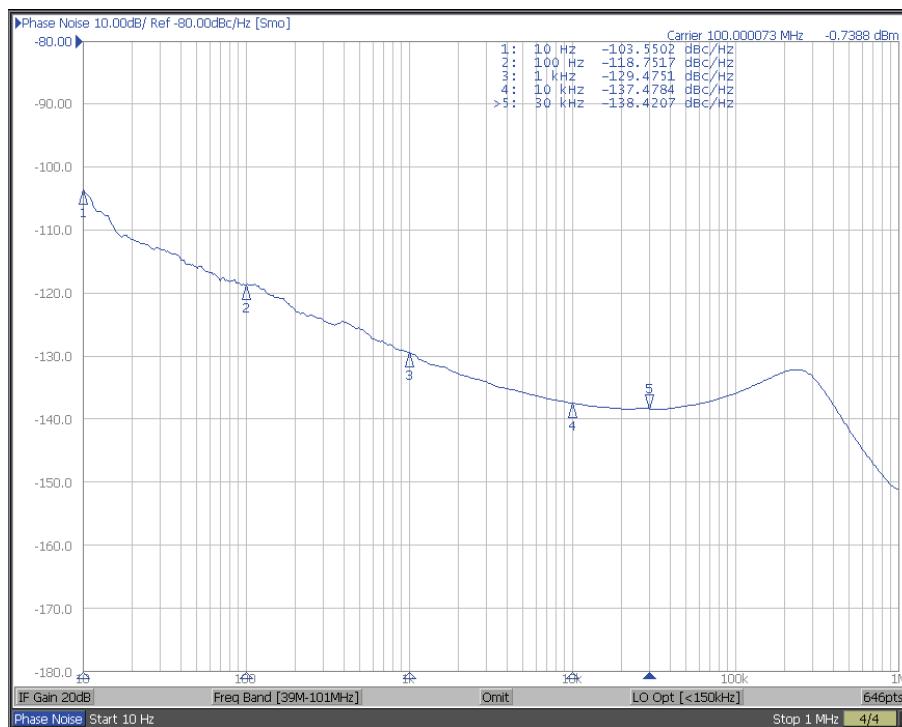
Note: * The phase detector PLL loop filter calculator and phase noise estimator spreadsheet can be downloaded at www.psemi.com.

Figure 3. Simulated Phase Noise Performance of the PE97420 at 100 MHz



From the estimated phase noise results, we would expect to achieve a normalized phase noise floor of -228 dBc/Hz. However, due to the slower edge rate of the 100 MHz sine wave, the actual measurement falls short of the expectation by achieving only -221 dBc/Hz as measured in *Figure 4*. Note that the VCO is the major wideband phase noise contributor and requires low phase noise.

Figure 4. Measured Phase Noise Performance Using a 100 MHz VCO with Sine Wave Output



To overcome the degraded phase noise performance, a low noise buffer is inserted at the VCO output as shown in *Figure 5*. The intent of the buffer is to increase the slew rate of the 100 MHz sine wave with minimal additive noise. The buffer used in this example is the LTC6957 from Linear Technology*. The LTC6957 is a very low phase noise, dual output AC signal buffer/driver/logic level translator. The LTC6957-4 option provides CMOS logic, complementary outputs and is available in a demo board.

Note: *The LTC6957 is used for demonstration purposes only and is not recommended for space-qualified applications.

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Figure 5. Block Diagram of 100 MHz Test Circuit Showing VCO Buffered Output

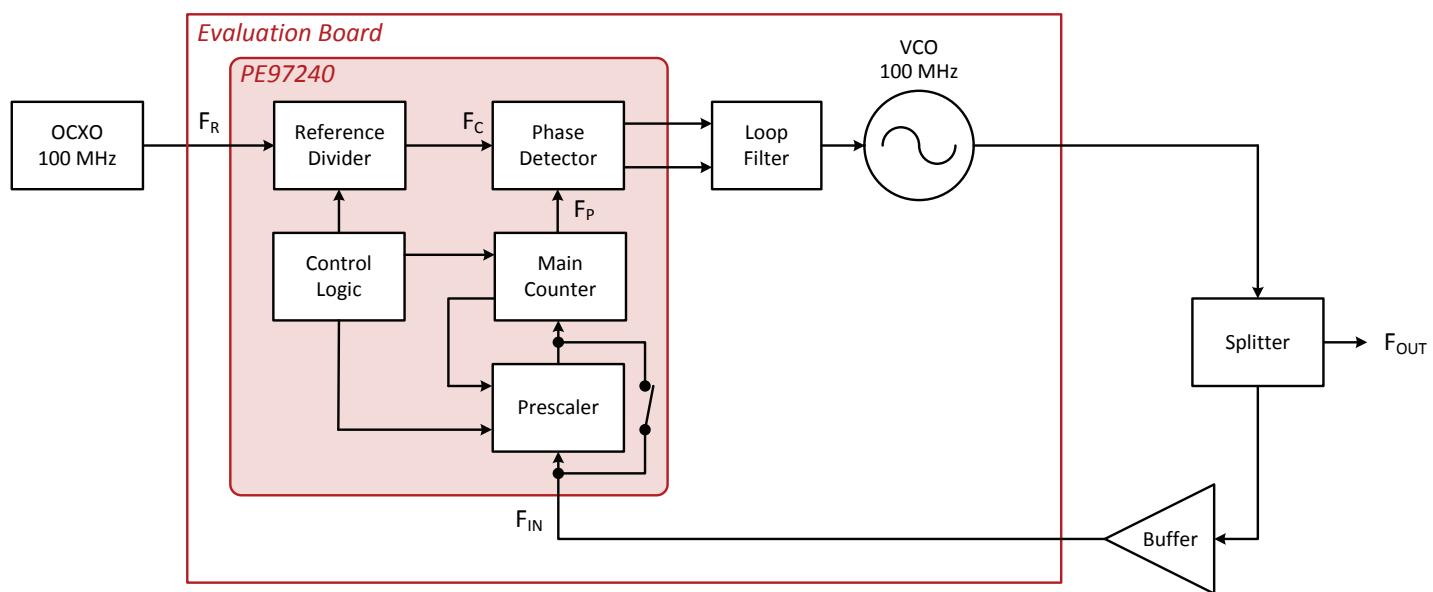
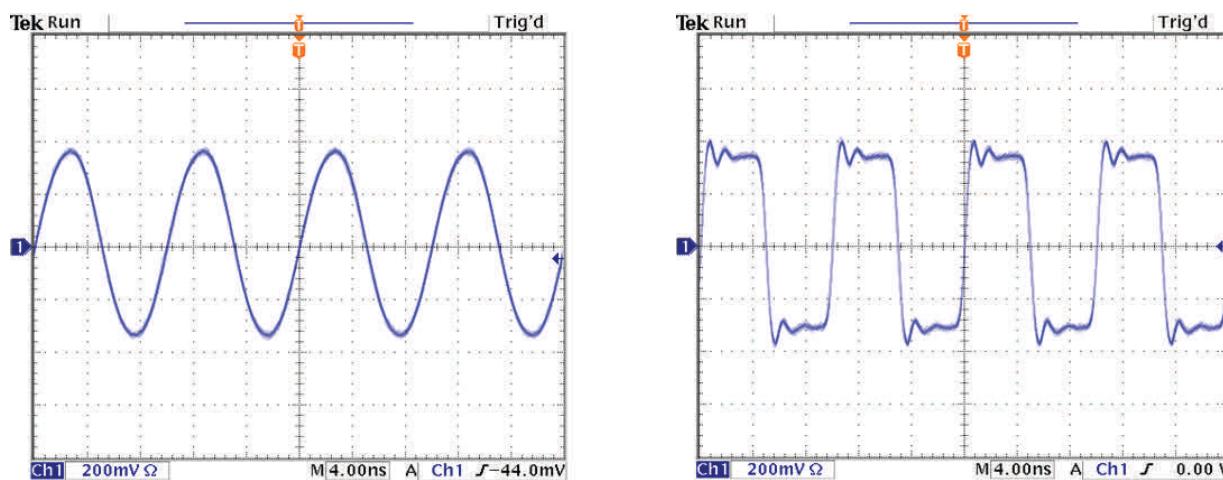


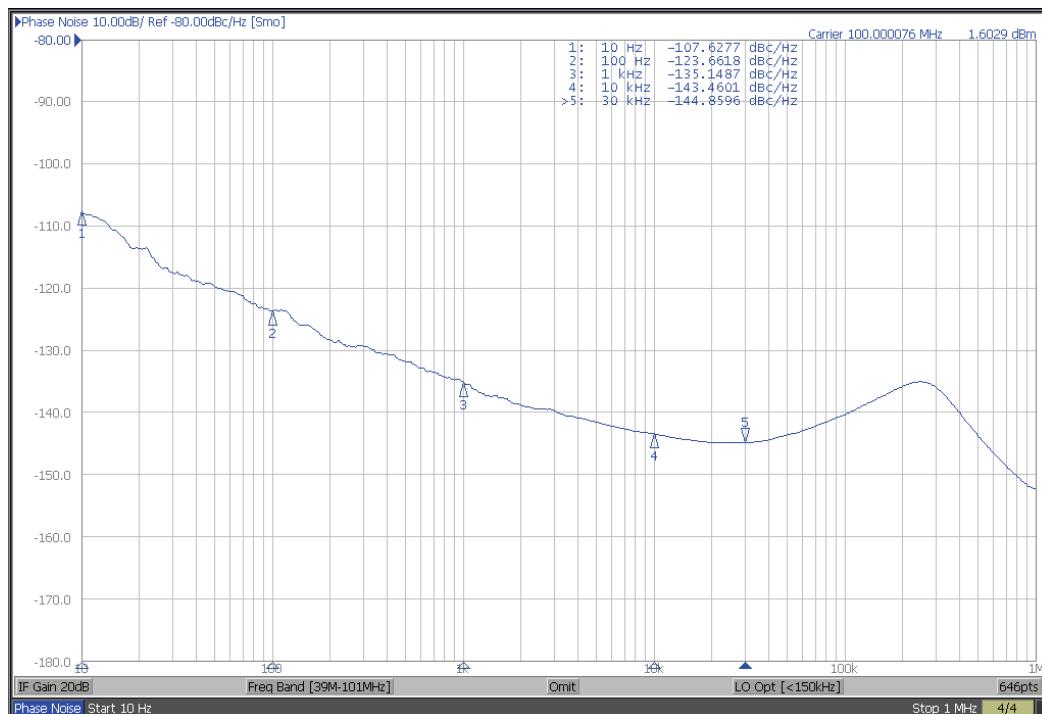
Figure 6 demonstrates the measured performance of the LTC6957-4 with a 100 MHz input sine wave and the resulting buffered output with faster edge rates.

Figure 6. LTC6957-4 Waveforms Showing a) 100 MHz Sine Wave Output and b) Buffered Output



The measured phase noise results in *Figure 7* indicate that the LTC6957-4 provides sufficient slew rate to the F_{IN} input. Additionally, the low additive phase noise of the LTC6957-4 has minimal impact on the PE97240 phase noise performance.

Figure 7. Measured Phase Noise Performance Using a 100 MHz VCO with a Buffered Output



Test Circuit Description

The simplified schematic of the PE97240 PLL with the LTC6957-4 demo board supplying the buffered VCO output is illustrated in *Figure 8*. An ultra-low noise OCXO is used as the reference source to ensure that the reference noise does not limit the phase noise measurements. The loop filter component values were determined from the PLL loop filter calculator and phase noise estimator spreadsheet as previously mentioned. The VCO with decent phase noise performance is readily available off the shelf. However, there is some wide band noise associated with the peaking response in the phase noise measurements. The power splitter and buffer are external to the PE97240 evaluation board. Note that it is also possible for the buffer to drive the RF input ports of the PE97240 differentially.

Figure 8. Simplified Schematic of PE97240 100 MHz Test Circuit with a Buffered VCO Output

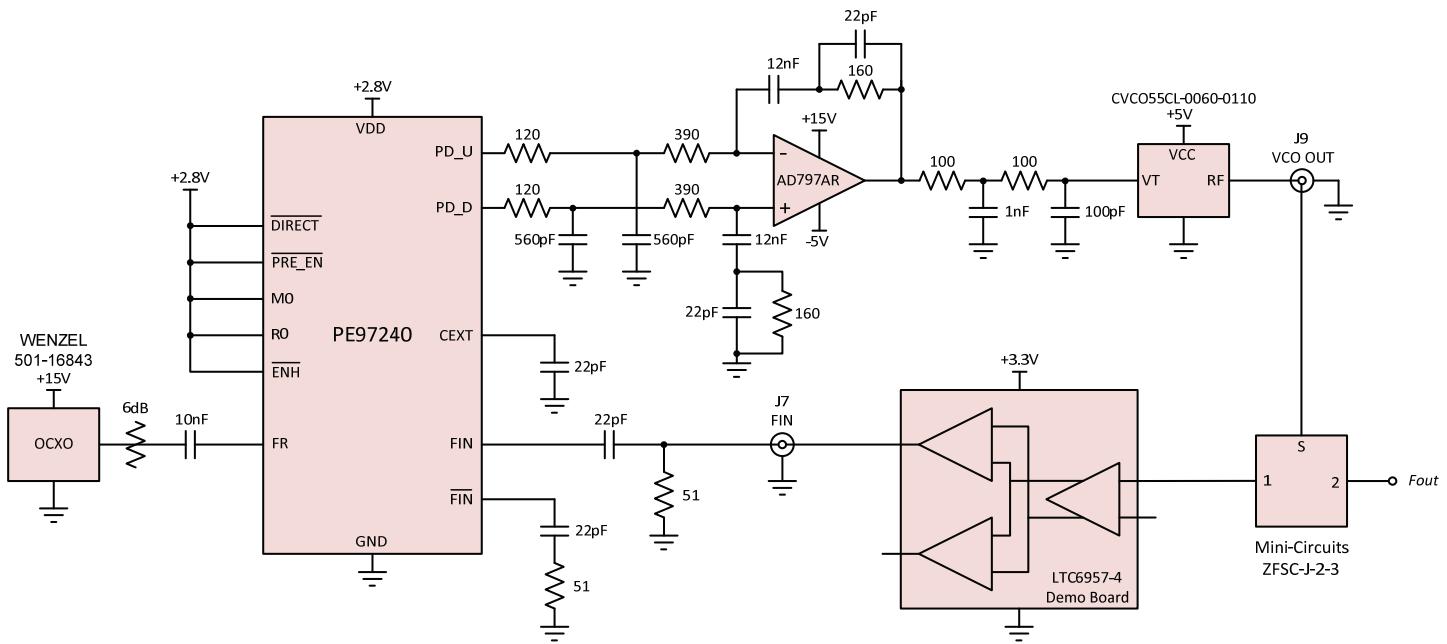


Figure 9 shows both the phase noise plots and the improvement obtained by improving the RF input slew rate with the buffer. The comparative normalized phase noise results are shown in Table 1.

Figure 9. Combined Phase Noise Plot Showing Improved Performance at 100 MHz

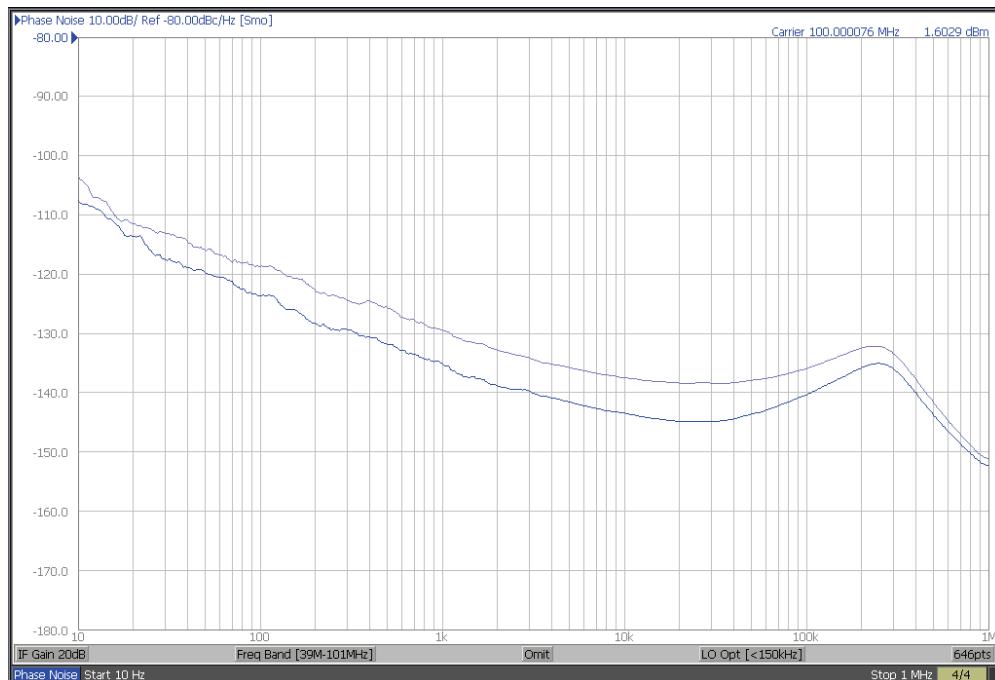


Table 1. Comparative Phase Noise Results of 100 MHz Test Circuit

RF Input Source	F_{IN} (MHz)	F_C (MHz)	N	Phase Noise @ 30 kHz Offset (dBc/Hz)	Normalized Phase Noise Floor (dBc.Hz)
Sine	100	50	2	-138.4	-221.41
Square	100	50	2	-144.8	-227.81

Conclusion

The circuit examples presented demonstrate the limitations of low RF input frequency operation of PLLs. RF signals with slower edge rates can critically degrade phase noise performance due to restrictions of the prescaler. In such cases, increasing the slew rate of the RF signal offers a solution where ultra-low phase noise is required.

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